Impact Evaluations

Air Contaminant	Difference in Project Emissions (lb/hr)	(k)(3)(C) Demonstration Limit (lb/hr)	Difference in Project Emissions Less Than Limit?	Applicable Distance (ft)	Applicable Distance > 1 mile?	Further Compliance Demonstration Necessary?				
Benzene	0.03	0.039	Yes	3,000	No	No				
H ₂ S	0.26	0.025	No	50	No	Yes				
SO ₂	7.42	2.00	No	50	No	Yes				
NOx	15.84	4.00	No	50	No	Yes				
There are no receptors within a mile of the site; therefore, benzene impacts are not included. Impacts for NO2, SO2, and H2S are included.										

H₂S Compliance Demonstration

Basis: This tab demonstrates compliance with the H₂S State Ambient Air Quality Standard (SAAQS) emission limitations in accordance with (k)(6)(A) & (B) of the non-rule Barnett Shale Standard Permit dated 11/08/2012.

Method Used	Emax
Short-term H ₂ S SAAQS (µg/m ³)	108
Background H ₂ S Concentration ¹ (µg/m ³)	0

Impacts	py Source:									<u>Method</u> S Demonstration ³
EPN	FIN	Emission Source	Horsepower	Stack Height (ft)	Distance to Property Line (ft)	Modeling Value ² (µg/m ³) / (lb/hr)	Modeling Table Category	Hourly H2S Emissions (lb/hr)	Wr (weighted ratio of emissions)	Maximum Allowable H2S Emissions (lb/hr)
FUG	FUG	Fugitive Emissions: Equipment Leaks		3	50	4375	Fugitive	0.04	15.33%	0.00
TL1	TL1	Condensate Loading		10	50	1232	Loading	0.01	5.11%	0.00
TL2	TL2	Water Loading		10	50	1232	Loading	0.01	5.11%	0.00
Sweet Flare	FL-1, TK1, TK2, TK3, GB1	Sweet Flare		20	50	58	Flares and Thermal Destruction Devices	0.15	56.32%	1.05
Sour Flare	FL-2, TK4, TK5, PIG	Sour Flare		20	50	58	Flares and Thermal Destruction Devices	0.05	18.12%	0.34
							Totals	0.26	100.00%	1.40

¹The background concentration of H₂S is expected to be negligible. In addition, there is no requirement to include background levels of H₂S in compliance demonstrations.

²Modeling values were chosen from the TCEQ Oil and Gas Emission Calculation Spreadsheet (Revised 10/2/2014), using the most conservative distance and applicable stack height (lowest value, highest impacts). ³H₂S is regulated by 30 TAC 112 on an hourly basis only (i.e., no annual compliance demonstration is required).

Equations used:

A. For Emax Method, Per Source: (Weighted Ratio, %) = (Actual Emissions from Source, lb/hr or tpy) / (Sum of all Sources, lb/hr or tpy)

B. For Emax Method, Per Source: (Maximum Allowable Emissions, lb/hr) = (Weighted Ratio, %) x (Short-term $H_2SSAQS, \mu g/m^3)$ / (Modeling Value, $\mu g/m^3$ per lb/hr)

C. For Predicted Impact Method, Per Source: (Predicted Concentration, $\mu g/m^3$) = (H₂S emissions, lb/hr) x [Modeling Value, ($\mu g/m^3$)/(lb/hr)]

Site-Wide Impacts:

Emax Method:	Hourly Demonstration
H ₂ S Emissions from All Sources (lb/hr)	0.26
Maximum Allowable H ₂ S Emissions (lb/hr)	1.40
Compliance Demonstrated? (Emissions < Allowable)	Yes

NO₂ Compliance Demonstration

Basis: This tab demonstrates compliance with the NO₂ National Ambient Air Quality Standard (NAAQS) emission limitations in accordance with (k)(6)(A) & (B) of the non-rule Barnett Shale Standard Permit dated 11/08/2012.

Method Used	Emax
Short-term NO ₂ NAAQS (µg/m ³)	188

Impacts by So	mpacts by Source:							NO ₂ Emissions			Emax Method Hourly NAAQS Demonstration ³	
EPN	FIN	Emission Source	Horsepower	Stack Height (ft)	Distance to Property Line (ft)	Modeling Value ¹ (µg/m ³) / (lb/hr)	Modeling Table Category	Hourly NO _x Emissions (lb/hr)	Source NO ₂ :NO _x Ratio ²	Hourly NO ₂ Emissions (lb/hr)	Wr (weighted ratio of emissions)	Maximum Allowable NO ₂ Emissions (lb/hr)
COMP1	COMP1	Engine 1: CAT 3606 TALE	1,775	20	50	7	Eng. 1500 < hp ≤ 2000	2.74	0.2	0.55	20.91%	5.62
COMP2	COMP2	Engine 2: CAT 3606 TALE	1,775	20	50	7	Eng. 1500 < hp ≤ 2000	2.74	0.2	0.55	20.91%	6
COMP3	COMP3	Engine 3: CAT 3606 TALE	1,775	20	50	7	Eng. 1500 < hp ≤ 2000	2.74	0.2	0.55	20.91%	5.62
COMP4	COMP4	Engine 4: CAT 3606 TALE	1,775	20	50	7	Eng. 1500 < hp ≤ 2000	2.74	0.2	0.55	20.91%	5.62
COMP5	COMP5	Engine 5: CAT 3306TA	203	20	50	71	Engine ≤ 250 hp	0.45	0.2	0.09	3.42%	0.09
COMP6	COMP6	Engine 6: Cummins KTA19CGA	380	20	50	34	Eng. 250 < hp ≤ 500	0.42	0.2	0.08	3.20%	0.18
ENGMAINT	ENGMAINT	Engine Maintenance: All 1,775 hp engines		20	50	N/A	Eng. 1000 < hp ≤ 1500	0.00E+00	0	0.00E+00	0.00%	0.00E+00
FL-1	FL-1, TK1, TK2, TK3, GB1	Sweet Flare		20	50	58	Flares and Thermal Dest. Dev.	0.85	0.2	0.17	6.51%	0.21
FL-2	FL-2, TK4, TK5, PIG	Sour Flare		20	50	58	Flares and Thermal Dest. Dev.	0.42	0.2	0.08	3.22%	0.10
	Totals									2.62	100.00%	23

¹Modeling values were interpolated by the TCEQ Oil and Gas Emission Calculation Spreadsheet (Revised 10/2/2014), unless otherwise noted.

²Per Barnett Shale PBR 106.352 and non-rule Barnett Shale Standard Permit (k)(4)(A), for all evaluations of NO_X to NO₂ a conversion factor of 0.20 for 4-stroke rich and lean burn engines, 0.50 for 2-stroke engines, and 0.5 for diesel engines are used. For other source types used conversion factor of 0.80 (EPA Memo "Guidance Concerning the Implementation of the 1-hour NO₂ NAAQS for the PSD Program" June 29, 2010).

³Annual ambient air standard compliance demonstration is not needed for NO₂. This is consistent with the table called "ESLs and AAQS needed for impacts review" on the "Is Full Impacts Review Required" tab in the TCEQ oil and gas calculation spreadsheet, dated 10/2/2014, which only lists the hourly NO₂ NAAQS. This is also consistent with the "NO₂ Full Impacts" tab of the TCEQ oil and gas calculation spreadsheet, dated 10/2/2014, which states at the top that a full impacts review needs to be done for NO₂ on an hourly basis. The reason for this is that the hourly NO₂ NAAQS is more stringent than the annual NAAQS, meaning that if the hourly NAAQS is met, even with the worst case hourly emissions occurring every hour of the year, the annual NAAQS would still be met. To illustrate this, if the hourly PMO₂ NAAQS, using the modeling factor of 0.08 to convert the concentration of 188 micrograms per cubic meter, which is the same as the hourly NO₂ NAAQS, using the modeling factor of 0.08 to convert the concentration from an hourly basis to an annual basis, the result is 15.04 micrograms per cubic meter, which is less than the annual NO₂ NAAQS, 100 micrograms per cubic meter. The 0.08 factor is discussed in a cell comment on the "Is Full Impacts Review Required" tab in the TCEQ oil and gas calculation spreadsheet, dated 10/2/2014, which states "Note that an acceptable factor to go from 1-hr to annual concentration is 0.08, so the 1-hr concentration may be multipide by 0.08 to get the annual NO₂. This is based on current, most stringent hourly and annual NO₂ ambient air quality standards as listed in the Technical Background Summary for the non-rule standard permit Effective February 2011 (P 57). If the standards are updated, this may change.

4. Engine Maintenance emissions for NOx are equal to normal operating emissions, and would not sum into maximum hourly totals.

Equations used:

- A. For Predicted Impact Method, Per Source: (Predicted Concentration, $\mu g/m^3$) = (NO₂ emissions, lb/hr) x [Modeling Value, ($\mu g/m^3$)/(lb/hr)]
- B. For Emax Method, Per Source: (Weighted Ratio, %) = (Actual Emissions from Source, lb/hr or tpy) / (Sum of all Sources, lb/hr or tpy)
- C. For Emax Method, Per Source: (Maximum Allowable Emissions, lb/hr) = (Weighted Ratio, %) x (Short-term NO₂ NAAQS, µg/m³) / (Modeling Value, µg/m³ per lb/hr)

Site-Wide Impacts:

Emax Method:	Hourly Demonstration
NO2 Emissions from All Source	s (lb/hr) 2.62
Maximum Allowable NO2 Emission	s (lb/hr) 23
Compliance Demonstrated? (Emissions < Al	owable) Yes

SO₂ Compliance Demonstration

Basis: This tab demonstrates compliance with the SO2 National Ambient Air Quality Standard (NAAQS) emission limitations in accordance with (k)(6)(A) & (B) of the non-rule Barnett Shale Standard Permit dated 11/08/2012.

Method Used	Emax
Short-term SO ₂ NAAQS (µg/m ³)	196

Impacts by Source:									sions <u>Emax Method</u> Hourly NAAQS Demonstratio	
EPN	FIN	Emission Source	Horsepower	Stack Height (ft)	Distance to Property Line (ft)	Modeling Value ¹ (µg/m ³) / (lb/hr)	Modeling Table Category	Hourly SO ₂ Emissions (lb/hr)	Wr (weighted ratio of emissions)	Maximum Allowable SO ₂ Emissions (lb/hr)
COMP1	COMP1	Engine 1: CAT 3606 TALE	1,775	20	50	7	Eng. 1500 < hp ≤ 2000	0.01	0.10%	0.03
COMP2	COMP2	Engine 2: CAT 3606 TALE	1,775	20	50	7	Eng. 1500 < hp ≤ 2000	0.01	0.10%	0.03
COMP3	COMP3	Engine 3: CAT 3606 TALE	1,775	20	50	7	Eng. 1500 < hp ≤ 2000	0.01	0.10%	0.03
COMP4	COMP4	Engine 4: CAT 3606 TALE	1,775	20	50	7	Eng. 1500 < hp ≤ 2000	0.01	0.10%	0.03
COMP5	COMP5	Engine 5: CAT 3306TA	203	20	50	71	Engine ≤ 250 hp	9.63E-04	0.01%	3.59E-04
COMP6	COMP6	Engine 6: Cummins KTA19CGA	380	20	50	34	Eng. 250 < hp ≤ 500	1.78E-03	0.02%	1.38E-03
ENGMAI NT	ENGMAINT	Engine Maintenance: All 1,775 hp engines		20	50	N/A	Eng. 1000 < hp ≤ 1500	0.00E+00	0.00%	0.00E+00
FL-1	FL-1, TK1, TK2, TK3, GB1	Sweet Flare		20	50	5.66	Flares and Thermal Dest. Dev.	5.58	75.34%	26.10
FL-2	FL-2, TK4, TK5, PIG	Sour Flare		20	50	58	Flares and Thermal Dest. Dev.	1.80	24.24%	0.82
		-			-		Totals	7.41	100.00%	27.03

¹Modeling values were interpolated by the TCEQ Oil and Gas Emission Calculation Spreadsheet (Revised 10/2/2014), unless otherwise noted.

²Annual ambient air standard compliance demonstration is not needed for SO₂. This is consistent with the table called "ESLs and AAQS needed for impacts review" on the "Is Full Impacts Review Required" tab in the TCEQ oil and gas calculation spreadsheet, dated 10/2/2014, which only lists the hourly SO₂ NAAQS. This is also consistent with the "SO₂ Full Impacts" tab of the TCEQ oil and gas calculation spreadsheet, dated 10/2/2014, which only lists the hourly SO₂ NAAQS. This is also consistent with the "SO₂ Full Impacts" tab of the TCEQ oil and gas calculation spreadsheet, dated 10/2/2014, which states at the top that a full impacts review needs to be done for SO₂ on an hourly basis. The reason for this is that the hourly SO₂ NAAQS is more stringent than the annual NAAQS, meaning that if the hourly NAAQS is met, even with the worst case hourly emissions occurring every hour of the year, the annual NAAQS would still be met. To illustrate this, if the hourly emissions are modeled to show a maximum off-property concentration of 196 micrograms per cubic meter, which is the same as the hourly SO₂ NAAQS, using the modeling factor of 0.08 to convert the concentration from an hourly basis to an annual basis, the result is 15.68 micrograms per cubic meter, which is less than the annual SO₂ NAAQS, 80 micrograms per cubic meter. The 0.08 factor is discussed in a cell comment on the "Is Full Impacts Review Required" tab in the TCEQ oil and gas calculation spreadsheet, dated 10/2/2014, which states "Note that an acceptable factor to go from 1-hr to annual concentration is 0.08, so the 1-hr concentration may be multiplied by 0.08 to get the annual Concentration." Note: This is based on current, most stringent hourly and annual SO₂ ambient air quality standards as listed in the Technical Background Summary for the non-rule standard permit Effective February 2011 (P 57). If the standards are updated, this may change.

4. Engine Maintenance emissions for SO2 are equal to normal operating emissions, and would not sum into maximum hourly totals.

Equations used:

A. For Predicted Impact Method, Per Source: (Predicted Concentration, $\mu g/m^3$) = (SO₂ emissions, lb/hr) x [Modeling Value, $(\mu g/m^3)/(lb/hr)$]

B. For Emax Method, Per Source: (Weighted Ratio, %) = (Actual Emissions from Source, lb/hr or tpy) / (Sum of all Sources, lb/hr or tpy)

C. For Emax Method, Per Source: (Maximum Allowable Emissions, lb/hr) = (Weighted Ratio, %) x (Short-term SO₂ NAAQS, µg/m³) / (Modeling Value, µg/m³ per lb/hr)

Site-Wide Impacts:

Emax Method:	Hourly Demonstration
SO ₂ Emissions from All Sources (lb/hr)	7.41
Maximum Allowable SO ₂ Emissions (lb/hr)	27.03
Compliance Demonstrated? (Emissions < Allowable)	Yes

*** SCREEN3 MODEL RUN *** *** VERSION DATED 13043 ***

C:\Users\Kat Galloway\OneDrive - brightskyenv.com\Client Files\Hilcorp\King Com

SIMPLE TERRAIN INPUTS:		
SOURCE TYPE	=	FLARE
EMISSION RATE (G/S)	=	0.125998
FLARE STACK HEIGHT (M)	=	6.0960
TOT HEAT RLS (CAL/S)	=	432693.
RECEPTOR HEIGHT (M)	=	0.0000
URBAN/RURAL OPTION	=	RURAL
EFF RELEASE HEIGHT (M)	=	8.3505
BUILDING HEIGHT (M)	=	0.0000
MIN HORIZ BLDG DIM (M)	=	0.0000
MAX HORIZ BLDG DIM (M)	=	0.0000

THE REGULATORY (DEFAULT) MIXING HEIGHT OPTION WAS SELECTED. THE REGULATORY (DEFAULT) ANEMOMETER HEIGHT OF 10.0 METERS WAS ENTERED.

BUOY. FLUX = 7.174 M**4/S**3; MOM. FLUX = 4.375 M**4/S**2.

*** FULL METEOROLOGY ***

*** TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES ***

DIST (M)	CONC (UG/M**3)	STAB	U10M (M/S)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGMA Y (M)	SIGMA Z (M)	DWASH
15.	0.000	1	1.0	1.0	320.0	102.27	7.32	5.91	NO
100.	2.874	3	10.0	10.0	3200.0	17.74	12.61	7.68	NO
200.	5.523	3	8.0	8.0	2560.0	20.09	23.86	14.42	NO
300.	5.098	4	10.0	10.0	3200.0	17.74	22.77	12.39	NO
400.	4.737	4	8.0	8.0	2560.0	20.09	29.64	15.63	NO
500.	4.182	4	5.0	5.0	1600.0	27.13	36.54	19.07	NO
600.	3.947	4	5.0	5.0	1600.0	27.13	43.05	21.88	NO
700.	3.621	4	4.5	4.5	1440.0	29.22	49.55	24.76	NO
800.	3.338	4	4.0	4.0	1280.0	31.83	55.98	27.61	NO
900.	3.096	4	3.5	3.5	1120.0	35.18	62.36	30.45	NO
1000.	2.876	4	3.0	3.0	960.0	39.66	68.71	33.32	NO
1100.	2.692	4	3.0	3.0	960.0	39.66	74.85	35.28	NO
1200.	2.515	4	3.0	3.0	960.0	39.66	80.94	37.18	NO
1300.	2.370	4	2.5	2.5	800.0	45.92	87.18	39.49	NO
1400.	2.247	4	2.5	2.5	800.0	45.92	93.17	41.28	NO
1500.	2.128	4	2.5	2.5	800.0	45.92	99.13	43.03	NO
1600.	2.173	5	1.0	1.0	10000.0	65.68	79.85	33.39	NO
1700.	2.235	5	1.0	1.0	10000.0	65.68	84.18	34.38	NO
1800.	2.283	5	1.0	1.0	10000.0	65.68	88.50	35.36	NO
1900.	2.321	5	1.0	1.0	10000.0	65.68	92.80	36.32	NO
2000.	2.348	5	1.0	1.0	10000.0	65.68	97.09	37.28	NO
2100.	2.355	5	1.0	1.0	10000.0	65.68	101.36	38.13	NO
2200.	2.355	5	1.0	1.0	10000.0	65.68	105.61	38.97	NO
2300.	2.367	6	1.0	1.0	10000.0	55.92	73.54	27.01	NO
2400.	2.412	6	1.0	1.0	10000.0	55.92	76.34	27.48	NO
2500.	2.451	6	1.0	1.0	10000.0	55.92	79.12	27.95	NO
2600.	2.485	6	1.0	1.0	10000.0	55.92	81.90	28.41	NO
2700.	2.514	6	1.0	1.0	10000.0	55.92	84.67	28.87	NO

3000. 3500. 4000. 4500. 5000. 5500. 6000. 6500. 7000. 7500. 8000. 8500. 9000. 9500. 10000.	2.557 2.504 2.432 2.349 2.261 2.173 2.086 2.002 1.917 1.838 1.763 1.693 1.628 1.567 1.119 0.8599 0.6951 0.5813 0.4382	6 6	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10000.0 100	55.92 55.92	92.92 106.52 119.94 133.20 146.30 159.27 172.12 184.84 197.46 209.98 222.40 234.73 246.98 259.15 271.24 388.67 501.13 609.90 715.72 920.32	$\begin{array}{c} 29.77\\ 30.21\\ 32.01\\ 33.70\\ 35.29\\ 36.81\\ 38.25\\ 39.64\\ 40.97\\ 42.25\\ 43.35\\ 44.41\\ 45.44\\ 46.43\\ 47.40\\ 48.33\\ 56.54\\ 61.81\\ 66.26\\ 70.16\\ 75.72 \end{array}$	NO NO NO NO NO NO NO NO NO NO NO NO NO N	
		UTRATION AT				111/.J1	00.33	NO	
		3 1				20.73	12.51	NO	
DWASH=NO DWASH=HS DWASH=SS	DWASH= MEANS NO CALC MADE (CONC = 0.0) DWASH=NO MEANS NO BUILDING DOWNWASH USED DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3*LB								
* * *	SUMMARY OF	* * * * * * * * * * * * * * * * * * *	EL RESULTS	***					
PROCEDU	RE	MAX CONC (UG/M**3)	MAX (M)	HT (M)					
SIMPLE TE		5.658			-				